



Modeling for plug-and-play control in strongly coupled nonlinear networks

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Intro

- Many real-world network systems (electric power grids, coupled robotic systems, biological systems) are becoming more strongly coupled than in the past; coupling is both temporal and spatial
- A basic question: Can coupling can be used for systematic design of cooperative control?
- Can't apply SSP modeling for near-optimal composite control design (temporal simplifications)
- Cant apply NSSP modeling for spatial simplifications
- Relevant because of implications on complexity and performance of control/communication designs
- Potential of controllers in the nodal components of the network, as well as potential of fast switched control of its branch components



Problem description

Three controllers (governor, Exciter and FACTS)

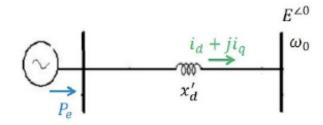


Fig.1 Electric power network

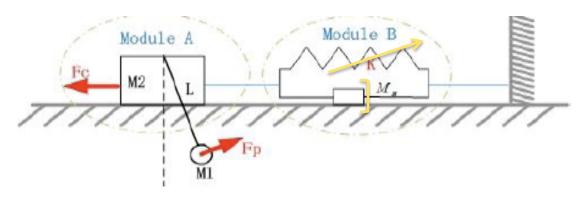


Fig. 2 Mechanical analogy of the electric power network

❖Three controllers (Fp, Fc, and controllable inerter)



Modeling questions for plug-and-play control design

- Control problem—strong coupling of modules A and B; MIMO design so that
- 1) pendulum is synchronized; 2) states and control within the pre-specified limits

Mechanical system modeling options

The standard state space model is

$$\dot{X}_A = f(X_A, X_B, u_A) \qquad X_A = [\theta \quad \omega \quad x_2 \quad v_2]^T \qquad U = [u_A \quad u_B]^T \qquad u_A = [F_P \quad F_C]^T$$

$$\dot{X}_B = f(X_B, X_A, u_B) \qquad X_B = [x_B \quad v_B]^T \qquad U = [u_A \quad u_B]^T \qquad u_B = [K]$$

❖Acceleration as the coupling (interaction) variable of modules A and B

$$\dot{\mathbf{X}}_{\text{pendulum}} = \mathbf{f}\left(\mathbf{X}_{\text{pendulum}}, \dot{\mathbf{v}}_{2}, \mathbf{u}_{p}\right)$$
 where u_{p} is F_{p}

$$\dot{\mathbf{X}}_{M2} = \mathbf{f}(\mathbf{X}_{M2}, \dot{\boldsymbol{\omega}}, \dot{\mathbf{v}}_{B}, \mathbf{u}_{M})$$
 where u_{M} is F_{C}

Stored energy and rate of change of stored energy coupling (interaction) variable—new state space

$$Z_{A} = \frac{1}{2}J\omega^{2} + \frac{1}{2}m_{2}v_{2}^{2} + m_{1}gl(\cos\theta - 1) \text{ where } J = m_{1}l^{2} \qquad P_{A} = J\omega\dot{\omega} + m_{2}\dot{v}_{2}v_{2} - m_{1}gl\sin\theta$$

$$Z_{B} = \frac{1}{2}m_{B}v_{B}^{2} + \frac{1}{2}k(x_{B} - x_{0})^{2} \text{ where } x_{0} \text{ is inital length of spring}$$

$$P_{B} = m_{B}v_{B}\dot{v}_{B} + k(x_{B} - x_{0})x_{B}$$

The new state space takes on the form

$$X_{A}^{\text{new}} = \begin{bmatrix} \overline{\overline{X}}_{A}^{T} & Z_{A} & P_{A} \end{bmatrix}^{T} \overline{\overline{X}}_{A} = \begin{bmatrix} \theta & \omega \end{bmatrix}^{T} \qquad X_{B}^{\text{new}} = \begin{bmatrix} Z_{B} & P_{B} \end{bmatrix}$$

$$\dot{\bar{X}}_A = f_A\left(\bar{\bar{X}}_A, Z_A, P_A, u_A\right)$$

$$\dot{Z}_A = f_{ZA}\left(\bar{\bar{X}}_A, Z_A, P_B\right)$$

$$\dot{P}_A = f_{PA}\left(\bar{\bar{X}}_A, P_A, \dot{P}_B\right)$$
Internal dynamics module A
$$\dot{Z}_B = f_{ZB}\left(Z_B, P_A, u_B\right)$$

$$\dot{Z}_B = f_{ZB}\left(Z_B, P_A, u_B\right)$$
terms of Interaction variables
$$\dot{P}_B = f_{PB}\left(P_B, \dot{P}_A\right)$$

Internal dynamics module A

$$\dot{\mathbf{Z}}_{B} = f_{ZB} \left(\mathbf{Z}_{B}, \mathbf{P}_{A}, u_{B} \right)$$

$$\dot{\mathbf{P}}_{B} = f_{PB} \left(P_{B}, \dot{P}_{A} \right)$$

Comparison of modular models

- ❖ Acceleration as an interaction variable works w/o assumptions if actuator dynamics are neglected; otherwise, projection of centrifugal force effect on M2 needs to be ignored; conjecture—if dynamics of actuator accounted for only stabilization around stable pendulum position possible; also acceleration must be communicated, hard to do
- When stored energy and rate of stored energy used as coupling (interaction) variables —no approximations needed; can stabilize around inverted pendulum (Furuta, Astrom)
- only local power measurement needed, completely decentralized
- It is possible to specify interactions over several time horizons
 —important for complex networks



Open problem

- Extend nonlinear control design to multi-layered strongly coupled complex networks.
- Provable performance precludes solutions in which position changes in an unbounded way
- New problem, when assumptions are not made (acceleration ideal input)
- Motivation--- functional specifications for interconnected smart grids with lots of fast power electronics switching; micro-grids; systems with wind power plants and delivery power electronically controlled to increase dellivery

